

Wide-Field Interferometric Imaging:

A Powerful Tool for the Terrestrial Planet Finder

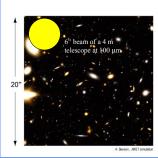
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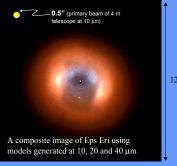
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Abstrac

We present a discussion of the design and construction of the Wide-Field Imaging Interferometry Testbed (WIIT) at the Goddard Space Flight Center. The testbed is motivated by a need to develop techniques for wide-field interferometric imaging in the optical/IR for future space missions such as TPF. Theoretically, using multipixel detectors for spatial multiplexing/mosaicing allows this, but in practice there are a number of questions which WIIT will address. We present some initial data acquired with this system and demonstrate its capability to produce wide-field interferometry data.

Motivation





"To ensure a broad science return from TPF, the committee recommends that, in planning the mission, comparable weight be given to the two broad science goals: studying planetary systems and studying the structure of astronomical sources at infrared wavelengths." (from the Decadal Report). The Wide-Field Imaging Interferometry Testbed was originally conceived to develop techniques and tools necessary for wide field-of-view interferometric imaging with FIR/Sub-mm missions such as SPECS (Submillimeter Probe of the Evolution of Cosmic Structure). For extragalactic surveys and studies of star formation regions, the small FOV inherent to Michelson stellar interferometers is insufficient, so techniques for wide FOVs are necessary. Similarily, in order to image star formation regions, debris disks, and to explore Origins themes, an interferometric TPF requires wide FOV techniques. The figure at the above right shows a model of the Eps Eri debris disk (he planet is marked by the + sign). In order to image the disk using an interferometric TPF (with 4-m telescopes) would require over 400 separate pointings! Using the techniques being explored with WIIT, the FOV could be enlarged by an areal factor of over 10000, thereby allowing observation of such a debris disk in a single pointing.

Testbed Performance

	Parameter Specification		Visibility		Table 2: Sources of Visibility Uncertainty in WIIT					
Source	Design Spec	Achieved	Formula	Value	Table 2: Sources of Ventury Constrainty in Will				Decert	ainty at
Alignment					Source	Parameter	Value	Formula	(Imar)	(Into)
Coalignment at Pupil Plane	>95% overlap	97.5%	1 - m	0.975	Camera		10000	- Continue	(Allegar)	(rein)
Tip/Tilt at Exit Pupil	<0.5 arcsec	0.5 arcsec	2J ₁ (* Du/\(\lambda\)	(0.988) ^a	Bit Noise	mu.	0.5	que/Nores	0.0033	0.025
Optics					Photon Counting	Notes	10000	$\sqrt{(2/N_{eler}) + (2^{n}/N_{ente})}$	0.0185	0.0253
Collimating Mirror					Carrera noise	Gen.	0.66	20 de el Nove	0.0088	0.0163
Surface roughness	15.75 mm		$e^{-(2\pi\delta/\lambda)}$	(0.98) **	(read noise, dark current)					
Beamsplitter					Turbulence					
Surface roughness	15 nm		$e^{-(2\pi\delta/\lambda)}$	(0.98) =	Wavefront distortion	Measured			0.05°	0.05
Interferometer Mirrors	Total Uncertainty in Measured Visibility									
Surface roughness	10 mm		$e^{-N(2\pi l/\lambda)}$	(0.92) a	Single Pixel					0.111
Combined observed effect				0.93	2x2 pixels					0.078
(Option & Tilt)					Tablenotes:					
Intensity Mismatch	>80% match	80%	$2/(\rho^{1/2} + \rho^{-1/2})$	0.994	a: Parentheses indicate that this parameter is rolled into measured values.					
Positional Knowledge	20 mm	9.89 mm	NCb	0.998						
Frame Expresse Time	<20 ms	<10 ms	NCb	0.99995	 b: NC indicates a numerically calculated quantity. 					
Total Predicted Visibility				0.905	c: Estimated values based on preliminary data.					

The tables above enumerate the sources of visibility loss in WIIT and sources of uncertainty in measured visibilities. The dominant effect in both cases is distortion of the wavefront due to optical surface errors and turbulent effects. Because WIIT operates at visible wavelengths in atmosphere, these effects are not comparable to sources of uncertainty in future interferometric space missions.

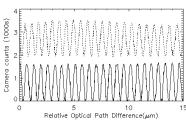
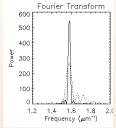
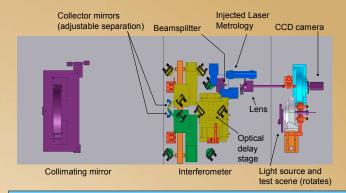


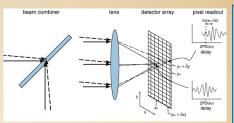
Table 1: Sources of Visibility Loss in WIII



The plot on the far left shows laser fringes acquired by WIIT with open-loop (dotted) and closed-loop (solid) metrology. The improvement provided by closed loop metrology is clear, especially in the Fouriet transform of the fringes in the plot on the near left.



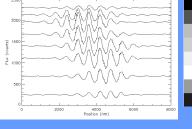
Layout of the Wide-Field Imaging Interferetry Testbed (WIIT). The testbed is designed to provide proof-of-concept of wide-field imaging interferometry. The source (on right) illuminates the collimator. The collimated beam returns to the two collector mirrors, and travels through a series of flat mirrors to the beam combiner. One of the two output ports of the interferometer continues to the science camera. To provide optical delay, one of the two arms of the interferometer uses a high-precision linear stage with two flat mirrors in a rooftop configuration. Full u-v plane coverage is provided by adjusting the baseline length and rotating the source scene.



The principle of wide-field imaging is relatively straightforward. A source on the sky appears on a pixel (x_o, y_o) , and as the delay line scans through Zero Path Difference (ZPD), the series of images produce an interferogram on the pixel in the time domain. For a second source separated by some angular offset, the image appears on a pixel $(x_o + \delta x, y_o)$, where $\delta x = f_{im0}$. The delay line scan produces an interferogram here as well, but with a shift in the ZPD of the interferogram.



Demonstration of Wide Field-of-View

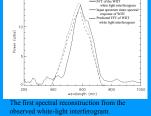


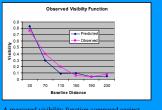


This series of three plots show the results of some of our early data from observing a 20 µm pinhole with no bandpass filter. The data are in good agreement with predictions. One plot of the creating of the control o









A measured visibility function compared against the predicted function.

References:

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